1 SAT - SISTA 18 - 45

Proceedings of the

1993 American Control Conference

The Westin St. Francis Hotel, San Francisco, California June 2-4, 1993

Sponsoring Organization

The American Automatic Control Council

U.S. National Member Organization of the

International Federation of Automatic Control (IFAC)

MEMBER ORGANIZATIONS

American Institute of Aeronautics and Astronautics
American Institute of Chemical Engineers
Association of Iron and Steel Engineers
American Society of Mechanical Engineers
Institute of Electrical and Electronic Engineers
Instrument Society of America
Society of Computer Simulation

The 1993 ACC is held in cooperation with IFAC

Volume 1 of 3



H_2 controller design with an H_∞ bounded controller

Johan David² Bart De Moor³

Department of Electrical Engineering Katholieke Universiteit Leuven Kardinaal Mercierlaan 94 B-3001 Leuven Belgium tel: ++32/16/220931 fax: ++32/16/221855 email: david@esat.kuleuven.ac.be demoor@esat.kuleuven.ac.be

Abstract

In this paper the minimization of an H_2 norm is considered, when the controller is restricted to be linear, stable, finite dimensional and H_{∞} -norm bounded. It is also shown how this can be used in the design of a mixed H_2/H_{∞} controller.

1 Introduction

In recent years there has been a lot of interest in the mixed H_2/H_{∞} design problem (e.g. [1]-[6]). This problem is stated as minimizing an H_2 -norm subject to the constraint that an H_{∞} -norm inequality has to be satisfied. In most papers, however, not the real H_2 -norm is minimized but an upper bound. In this paper an other problem is considered first. The H_2 -norm of a transfer function should be minimized using a linear, stable, finite dimensional controller that satisfies an H_{∞} -bound. Necessary conditions for this problem are derived, using a parameterization of this set of controllers of Steinbuch and Bosgra [5]. This can then be used to find controllers of a certain finite dimension that minimize a H_2 -norm subject to a H_{∞} -norm constraint, as in the case of the general mixed H_2/H_{∞} design problem.

2 Parameterization of H_{∞} norm bounded transfer functions

In [5] Steinbuch and Bosgra describe a parameterization for strictly proper, stable, norm-bounded finite dimensional transfer functions: Let the set Ω^*_{γ} be defined as

$$\Omega_{\gamma}^{\bullet} = \{F(s) \mid ||F(s)||_{\infty} < \gamma, F(s) \text{ stable, real rational,}$$

strictly proper and of McMillan degree $\leq n\}$ and consider the set Ω_{γ}

$$\Omega_{\gamma} = \{C(sI - A)^{-1}B|A = A_s + A_k, A_s = -\frac{1}{2}\gamma^{-2}BB^T$$

$$-\frac{1}{2}C^TC,\ A_k=-A_k^T\in\mathbb{R}^{n\times n},B\in\mathbb{R}^{n\times n_w},C\in\mathbb{R}^{n_s\times n}\}$$

Proposition 1 [5]: $\Omega_{\gamma} = \Omega_{\gamma}^{\bullet}$.

3 H_2 optimization with an H_{∞} bounded controller

In this section necessary conditions are derived for a H_{∞} -norm bounded controller that minimizes an H_2 -norm. We will call this problem a constrained H_2 problem. Consider the following linear, time invariant plant:

$$\dot{x} = Ax + B_1 w + B_2 u
z = C_1 x + D_{11} w + D_{12} u
y = C_2 x + D_{21} w + D_{22} u$$
(1)

Now find a dynamic, stable, strictly proper, H_{∞} -norm bounded controller K, u=Ky, that stabilizes the closed loop and such that the H_2 -norm of the closed loop transfer function from w to z is minimized. K has to belong to Ω_{γ} . Without loss of generality γ can be taken $\gamma=1$. The state space realization of the controller is then:

$$\dot{x}_c = A_c x_c + B_c y
 u = C_c x_c$$
(2)

To make the 2-norm of the closed loop finite, D_{11} has to be 0. For notational reasons, we also assume $D_{22} = 0$. This is not a limitation, as the controller is strictly proper. This is shown e.g. in the paper of Glover and Doyle on H_{∞} control [7].

From (1) and (2) the state space realization of the closed loop can be derived $(D_{11} = 0 \text{ and } D_{22} = 0)$:

$$\begin{pmatrix} \dot{x} \\ \dot{x}_c \end{pmatrix} = \begin{pmatrix} A & B_2 C_c \\ B_c C_2 & A_c \end{pmatrix} \begin{pmatrix} x \\ x_c \end{pmatrix} + \begin{pmatrix} B_1 \\ B_c D_{21} \end{pmatrix} w$$

$$z = \begin{pmatrix} C_1 & D_{12} C_c \end{pmatrix} \begin{pmatrix} x \\ x_c \end{pmatrix}$$

Define

$$\overline{A} = \begin{pmatrix} A & B_2 C_c \\ B_c C_2 & A_c \end{pmatrix} \qquad \overline{B} = \begin{pmatrix} B_1 \\ B_c D_{21} \end{pmatrix}$$

$$\overline{C} = \begin{pmatrix} C_1 & D_{12} C_c \end{pmatrix}$$

The control objective can be expressed as $\min_{K \in \Omega_1} \operatorname{trace}\{\overline{C}^t \overline{C}S\}$ where S is the solution of $\overline{A}S + S\overline{A}^t + \overline{B}\overline{B}^t = 0$. Necessary conditions for this problem are given in the following lemma:

Lemma 1 Necessary conditions for the constrained H₂ problem.

Given the state space realization of (1), a stable, finite dimensional, strictly proper controller K, with H_{∞} -norm smaller than 1, that stabilizes the closed loop

¹The following text presents research results obtained within the framework of the Belgian programme on interuniversity attraction poles initiated by the Belgian State - Prime Minister's Office - Science Policy Programming. The scientific responsibility is assumed by its authors.

ity is assumed by its authors.

2 Johan David is a research assistant with the N.F.W.O. (Belgian National Fund for Scientific Research).

³Bart De Moor is a research associate with the N.F.W.O.



and minimizes the H2-norm of the closed loop transfer function from w to z satisfies the following equations:

$$\overline{A}S + S\overline{A}^{t} + \overline{B}\overline{B}^{t} = 0$$

$$P\overline{A} + \overline{A}^{t}P + \overline{C}^{t}\overline{C} = 0$$

$$\left(\begin{array}{ccc} P_{12}^{t} & P_{22} \end{array}\right) \left(\begin{array}{c} S_{12} \\ S_{22} \end{array}\right) = \left(\begin{array}{ccc} S_{12}^{t} & S_{22} \end{array}\right) \left(\begin{array}{c} P_{12} \\ P_{22} \end{array}\right)$$

$$A_{t} + \frac{1}{2}B_{c}B_{c}^{t} + \frac{1}{2}C_{c}^{t}C_{c} = 0$$

$$B_{c} = \left[\left(\begin{array}{ccc} S_{12}^{t} & S_{22} \end{array}\right) \left(\begin{array}{c} P_{12} \\ P_{22} \end{array}\right)\right]^{-1} \left(\begin{array}{ccc} P_{12} & P_{22} \end{array}\right) \left(\begin{array}{c} S_{11} \\ S_{12}^{t} \end{array}\right) C_{2}^{t}$$

$$C_{c} \left(\begin{array}{ccc} S_{12}^{t} & S_{22} \end{array}\right) \left(\begin{array}{c} P_{12} \\ P_{22} \end{array}\right) - D_{12}^{t}D_{12}C_{c}S_{22}$$

$$= D_{12}^{t}C_{1}S_{12} + B_{2}^{t} \left(\begin{array}{c} P_{11} & P_{12} \end{array}\right) \left(\begin{array}{c} S_{12} \\ S_{22} \end{array}\right)$$

where $A_c = A_s + A_k$ with $A_s = A_s^t$ and $A_k = -A_k^t$. S and P have to be positive definite S > 0 and P > 0. The inverse has to exist.

The proof is straight forward using Lagrange multipli-

Application to the H_2/H_{∞} problem

Using the above solution for the constrained H2 problem with dynamic output feedback, the general mixed

H₂/ H_{∞} problem can also be solved. It is well-known that in general there is a set of solutions to the suboptimal H_{∞} control problem [7], [8]. If there exists a solution, of course. Without loss of generality the H_{∞} control problem can always be solved with that the H_{∞} control problem can always be solved. such that the H_{∞} -norm of the closed loop is smaller than 1. The set of controllers satisfying this condition is parameterized by a controller generator and a feedback Q. Where Q is a stable, H_{∞} -norm bounded transfer function.

This is used to solve the mixed H_2/H_{∞} control problem. The state space realization is:

$$\dot{x} = Ax + B_{w_1}w_1 + B_{w_2}w_2 + B_{u}u
z_1 = C_{z_1}x + D_{z_1w_1}w_1 + D_{z_1w_2}w_2 + D_{z_1u}u
z_2 = C_{z_2}x + D_{z_2w_1}w_1 + D_{z_2w_2}w_2 + D_{z_2u}
y = C_{y}x + D_{yw_1}w_1 + D_{yw_2}w_2 + D_{yu}u$$
(3)

Find a controller such that the closed loop from $(w_1 \ w_2)^t$ to $(z_1 \ z_2)^t$ is stable, $||T_{z_1w_1}||_2$ is minimized and $||T_{z_2w_3}||_{\infty} < 1$. The idea is now to calculate first the controller for the H_{∞} part of the problem. Thus check if the H_{∞} suboptimal problem is solvable, based on w_2 , u, z_2 and y. If so, the controller generator, that is also a generalized system, is attached to ator, that is also a generalized system, is attached to the plant (3). Now concentrate on the H_2 problem. Within the set of controllers that stabilize the closed loop and satisfy the H_{∞} condition $||T_{z_2w_2}||_{\infty} < 1$, find the controller that minimizes the H_2 -norm of $T_{z_1w_1}$. Therefore, we search for the transfer function Q, r = Qv, that minimizes the H_2 -norm from z_1 to w_1 . The transfer function Q, however, should be such that it doesn't destabilize $T_{z_1w_2}$ and keeps the H_{∞} -norm less than or equal to 1. Therefore, we know from the H_{∞} control theory, that Q has to be a stable transfer function such that $\|Q\|_{\infty} < 1$. To obtain a finite H_2 -norm the following conditions are needed:

1. $D_{i_1w_1} = 0$. 2. Q has to be strictly proper. A state space realization of Q is then:

$$\dot{x}_q = A_q x_q + B_q v$$
$$r = C_q x_q$$

Thus Q has to be stable, strictly proper and H_{∞} -norm bounded $||Q||_{\infty} < 1$. Thus Q has to be an element of Ω_1 . So, the procedure explained in section 3 can be applied. spined. Find $Q \in \Omega_1$, such that $T_{x_1w_1}$ is stable and $||T_{x_1w_1}||_2$ is minimized. The closed loop will be stable. This is ensured by the H_{∞} theory, if there is a stable solution $((A, B_u, C_y))$ has to be stabilizable and detectable). The H_{∞} and H_2 part have the same feedback loop. So, if $T_{x_2w_2}$ is stabilized so will be $T_{z_1w_1}$. From this derivation, it should also be clear that the lowest possible H_{∞} norm, is the lowest possible norm

lowest possible H_{∞} norm, is the lowest possible norm

that can be achieved for the H_{∞} -problem for $T_{z_2w_2}$.

Conclusions

In this paper we showed how the mixed H_2/H_{∞} problem can be solved over the set of linear finite dimensional controllers. It is possible to solve this problem by first solving an H_{∞} problem and then solving a constrained H_2 problem. Necessary conditions for the constrained H_2 problem are derived. Numerical calculation based on a quasi-Newton optimization give a satisfying result. However, due to space limitations these are not discussed further.

limitations, these are not discussed further.

References

- [1] D.S. Berstein and W.M. Haddad, "LQG control with H[∞] performance bound: A Riccati equation approach," IEEE Trans. Autom. Contr., vol. 34, pp. 293-305,1989.
- [2] J.C. Doyle, K. Zhou, and B. Bodenheimer, "Optimal control with mixed H_2 and H^{∞} performance objectives," *Proc. ACC*, Pittsburgh, PA, p. 2065-2070, 1989.
- [3] P.P. Khargonekar, and M.A. Rotea, "Mixed H_2/H_{∞} control: A convex optimization approach," *IEEE Trans. Autom. Contr.*, Vol. 36, pp. 824-837, 1991.
- [4] D. Mustafa, Minimum Entropy H_{∞} Control, PhD Thesis, University of Cambridge, 1989.
- [5] M. Steinbuch, and O. Bosgra, "Robust performance in H_2/H_{∞} optimal control," Proc. 30 CDC, Brighton, pp. 549-550, 1991.
- [6] H.-H. Yeh, S.S. Banda, B.-C. Chang, "Necessary and sufficient conditions for mixed H_2 and H_{∞} optimal control," IEEE Trans. Autom. Contr., vol. 37, pp. 355-358, 1992.
- [7] K. Glover and J.C. Doyle, "State-space formulae for all stabilizing controllers that satisfy an H_{∞} norm bound and relations to risk sensitivity, Syst. Contr. Lett., vol. 11, pp. 167-172, 1988.
- [8] K. Glover, D. Limebeer, J. Doyle, E. Kasenally, and M. Safanov, "A characterization of all solution to the H_{∞} four block problem," SIAM J. Control Optim., 29, pp. 283-324, 1991.